

# Mechanical properties of bovine articular cartilage under microscale indentation loading from atomic force microscopy

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**Abstract:** Atomic force microscopy (AFM) techniques have been increasingly used for investigating the mechanical properties of articular cartilage. According to the previous studies reporting the microscale Young's modulus under AFM indentation tests, the Hertz contact model has been employed with a sharp conical tip indenter. However, the non-linear microscale behaviour of articular cartilage could not be resolved by the standardized Hertz analysis using small and sharp atomic force microscope tips. Therefore, the objective of this study was to evaluate the microscale Young's modulus of articular cartilage more accurately through a non-Hertzian approach with a spherical tip of 5  $\mu\text{m}$  diameter, and to characterize its microscale mechanical behaviour. This methodology adopted in the present study was proved by the consistent values between the microscale (2 per cent, about 9.3 kPa; 3 per cent, about 17.5 kPa) and macroscale (2 per cent, about 8.3 kPa; 3 per cent, about 18.3 kPa) Young's moduli for 2 per cent and 3 per cent agarose gel ( $n = 100$ ). Therefore, the microscale Young's modulus evaluated in this study is representative of more accurate measurements of cartilage stiffness at the 600 nm deformation level and corresponds to approximately 30.9 kPa ( $n = 100$ ). Furthermore, on this level of the microscale deformation, articular cartilage showed depth-dependent and frequency-independent behaviour under AFM indentation loading. These findings reveal the microscale mechanical behaviour of articular cartilage more accurately and can be employed further to design microscale structures of chondrocyte-seeded scaffolds and tissue-engineered cartilage by evaluating their microscale properties.

**Keywords:** atomic force microscopy, cartilage mechanics, mechanical response, microscale indentation

## 1 INTRODUCTION

Atomic force microscopy (AFM) techniques have increasingly been used for measuring tribological and mechanical properties (i.e. surface roughness, wear, friction, elastic modulus, and boundary lubrication) of engineering and biological surfaces on nanoscale and microscale levels [1–6]. AFM tribological studies have been reported on many biological

surfaces (hydrogels, phospholipid co-adsorbed layers, dentin, enamel, dentino-enamel junction, and human hair) [7–12] as well as the cartilage surface [3, 13–15]. AFM indentation testing has also been widely used to calculate mechanical properties of soft materials by evaluating the elastic modulus  $E$  from the Hertz contact model [16–24]. However, these AFM indentation studies have been performed on the cells (human umbilical vein endothelial cells, liver epithelial cells, cardiac muscle cells, skeletal muscle cells, etc.) and biological fibres and have mainly focused on the spatial variations in their elastic moduli. By adopting the Hertz contact

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model, Mathur *et al.* [20] have reported an elastic modulus of about 7.2 kPa over the nucleus, about 3.0 kPa over the cell body in proximity to the nucleus, and about 1.3 kPa on the cell body near the edge. Costa *et al.* [25] have adopted a non-Hertzian approach because of the unrealistic assumptions of a simplified Hertz theory and reported the average pointwise moduli of approximately 5.6 kPa and approximately 1.5 kPa for two distinct populations of human aortic endothelial cells at an indentation depth up to 200 nm.

Regarding articular cartilage, the mechanical material properties have not yet been well characterized on microscale levels; neither have the relationships between microscale and macroscale mechanical properties. There are only limited AFM data for articular cartilage. Young's moduli  $E_Y$  of rabbit jaw condylar articular cartilage calculated by the Hertz contact model with an oxide-sharpened conical atomic force microscope tip (radius of curvature, about 20 nm) have been compared for neonatal tissue (about 0.9–1.0 MPa) and adult tissue (about 1.0–2.3 MPa) as well as for the anteromedial region (about 2.3 MPa) and the posterolateral region (about 1.0 MPa) [26, 27]. Most AFM studies in the literature have used small and sharp atomic force microscope tips for indentation testing on the soft materials including articular cartilage. Dimitriadis *et al.* [28] have shown that the most fundamental assumption of the Hertz contact model, i.e. small deformations or strains, is easily violated by sharp atomic force microscope cantilever tips, but spherical atomic force microscope cantilever tips can reduce the non-linearity of soft materials compared with sharp cantilever tips. These spherical atomic force microscope tips (2.5  $\mu\text{m}$  and 10  $\mu\text{m}$  radius) have been used to measure frictional coefficients of articular cartilage (about 0.15) [15], intertubular dentin (about 0.31) and enamel (about 0.14) [12] to minimize ploughing forces from plastic deformation. Moreover, the effective compressive modulus  $E^*$  of articular cartilage has been measured in a recent study with a spherical atomic force microscope tip (2.5  $\mu\text{m}$  radius) by three of the present authors [15] by curve fitting AFM indentation data with the Hertz contact model which gave  $E^* \approx 46$  kPa. However, because even the spherical atomic force microscope cantilever tips are not able to resolve the non-linear behaviour of articular cartilage completely on a microscale [15], another approach without using the standardized Hertz analysis is desirable to measure the microscale modulus of articular cartilage more accurately.

Therefore, the objective of the present study was to measure the microscale Young's modulus  $E_Y$  of articular cartilage more accurately by adopting a non-Hertzian approach [25] and using a relatively large spherical atomic force microscope tip. The second objective was to characterize the microscale mechanical response of articular cartilage.

## 2 MATERIALS AND METHODS

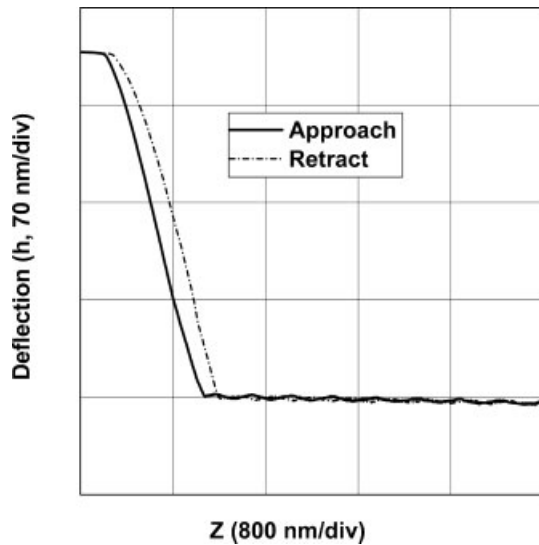
### 2.1 Sample preparation

Two cylindrical osteochondral plugs (diameter 8 mm,  $h \approx 1.5$  mm) were harvested from two fresh bovine humeral heads (2–4 months old). Using a sledge microtome (model 1400; Leiz, USA), approximately 1 mm of the tissue for AFM was taken from the deep zone to remove remnants of subchondral bone and vascularized tissue and to produce a surface parallel to the articular side, leaving the articular surface intact. Cartilage samples were refrigerated at 4 °C and tested within 3 days, but never frozen. In order to validate the microscale Young's moduli from AFM measurements by comparison with the macroscale Young's moduli, 2 per cent and 3 per cent (wt/vol) low-melt agarose hydrogels (type VII, Sigma Chemicals, USA) were also prepared.

### 2.2 Microscale AFM indentation experiment

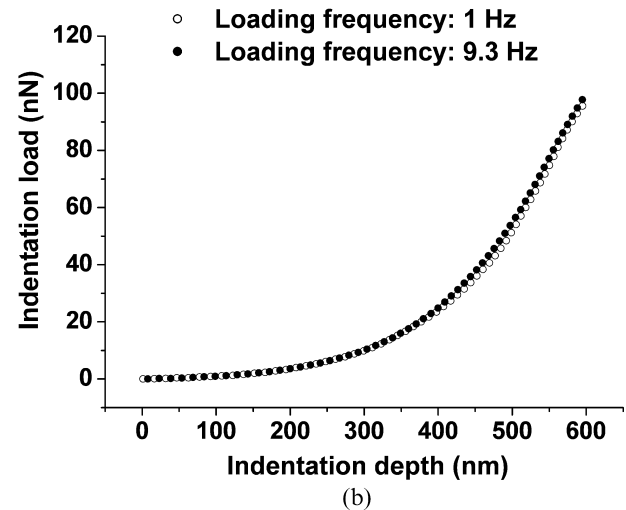
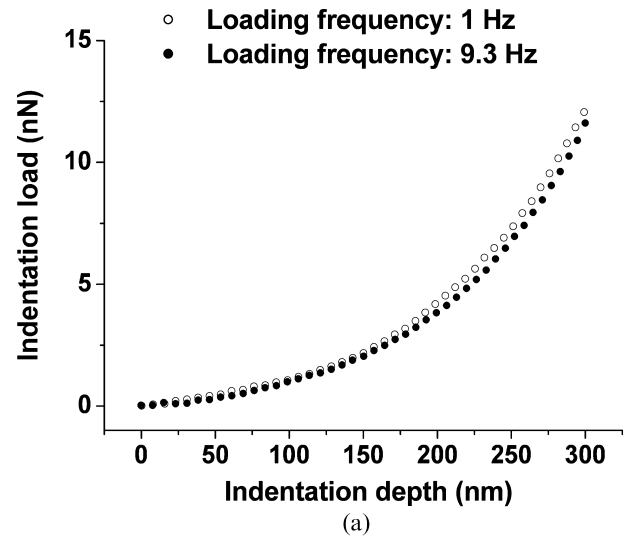
Samples (2 per cent and 3 per cent agarose gel; articular cartilage) for AFM indentation testing were glued on the bony side to 35 mm polystyrene petri dishes using a small amount of cyanoacrylate glue. AFM indentation testing was conducted with samples entirely submerged in phosphate-buffered saline (PBS) on a Bioscope atomic force microscope (Digital Instruments, USA) with  $Z$  limits for indentation of 2.5 V and 20 V (Fig. 1). Custom silicon nitride AFM probes with polystyrene spherical tips ( $R = 2.5$   $\mu\text{m}$ ; Novascan Technologies, USA) having a nominal spring constant of  $k = 0.32$  N/m were used for AFM indentation testing. The mounted probe was submerged in PBS for at least 20 min prior to imaging to allow for thermal equilibration at room temperature.

Before AFM indentation testing, the deflection sensitivity was determined in PBS on glass every time that the atomic force microscope cantilever probe was mounted on the atomic force microscope head, and it ranged from 41.17 nm/V to 63.86 nm/V. Approach signals from AFM indentation tests were



**Fig. 1** Typical profile of the approaching and retracting signals of AFM indentation loading on the surface of articular cartilage at 9.3 Hz loading frequency with a  $Z$  limit of 20 V

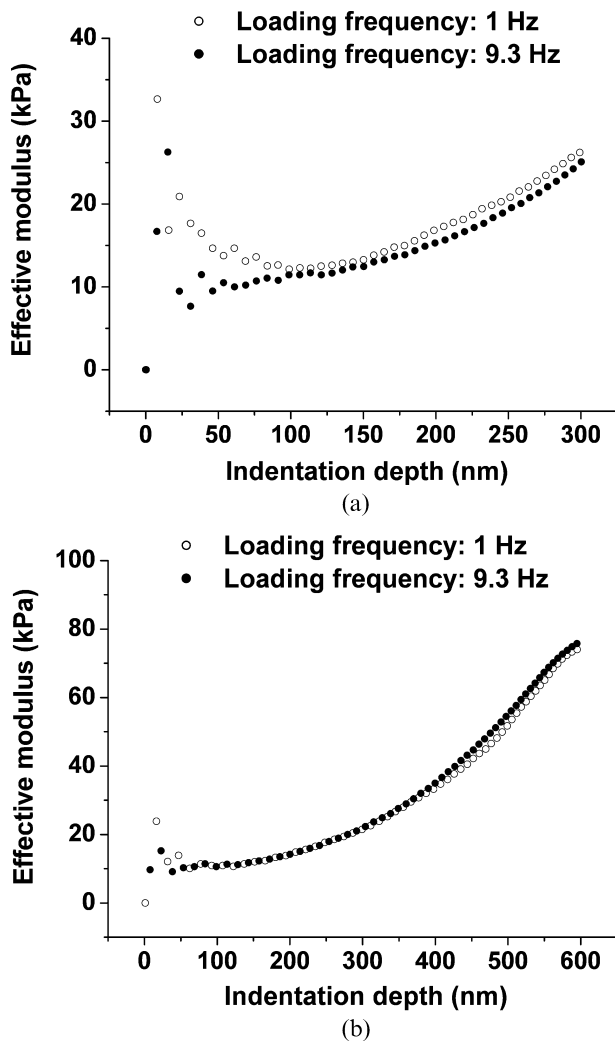
cantilever normal deflection  $h$  signals as a function of sample position height  $Z$  produced by Nanoscope III software obtained with the AFM device (Digital Instruments, USA). These approach signals were converted to the indentation depth  $D = Z - h$  versus indentation load  $F = kh$  curves (Fig. 2). Because the indentation depth  $D_i$  and load  $F_i$  of the  $i$ th data point were assumed to be related by the Hertz contact formula  $F_i = \frac{4}{3} E_i^* R_i^{1/2} D_i^{3/2}$ , the pointwise effective moduli  $E_i^*$  of each data point  $i$  for the indentation depth–load data were calculated by an equation of the form  $E_i^* = F_i / \left( \frac{4}{3} E_i^* R_i^{1/2} D_i^{3/2} \right)$  with  $R = 2.5 \mu\text{m}$  as shown in Figs 3, 4, and 5 [17, 23, 25, 29, 30]. These pointwise effective moduli  $E_i^*$  of each data point  $i$  were averaged over all data points of the indentation depth–load curve to obtain an average pointwise  $E^*$  over the indentation depth  $D = 300 \text{ nm}$  ( $Z$  limit, 2.5 V) and  $D = 600 \text{ nm}$  ( $Z$  limit, 20 V), instead of performing a least-squares fit of the measured indentation depth–load data with the Hertz contact formula to extract a single value of  $E^*$  from each indentation curve. The average pointwise effective modulus  $E^*$  over the indentation depth for each AFM measurement was converted to the average pointwise Young's modulus (i.e. the microscale  $E_Y$ ) from the equation  $E^* = E_Y / (1 - \nu^2)$  where Poisson's ratio  $\nu = 0.5$  [17, 23, 25, 29, 30]. To identify the ideal contact point between the atomic force microscope tip and the sample surface, a two-part polynomial model-fitting algorithm developed by Costa *et al.* [25] was adopted.



**Fig. 2** Typical profiles of cartilage indentation depth versus indentation load which were converted from the approaching signal of AFM indentation with the indentation depths of (a) up to 300 nm and (b) up to 600 nm

### 2.3 Microscale $E_Y$ of agarose gel and articular cartilage

AFM indentation tests were performed on each 2 per cent and 3 per cent (wt/vol) agarose hydrogel with a  $Z$  limit of 20 V at 1 Hz loading frequency. The microscale  $E_Y$  (i.e. the average pointwise  $E_Y$ ) over the indentation depth of 600 nm for each indentation depth–force curve was calculated from the pointwise  $E^*$  (Fig. 5) using the method explained above in order to compare these microscale  $E_Y$  values of 2 per cent and 3 per cent agarose gels with their macroscale  $E_Y$  values. The same experimental method was used for the cartilage samples, and then the microscale  $E_Y$  of articular cartilage was obtained ( $n = 100$ ).



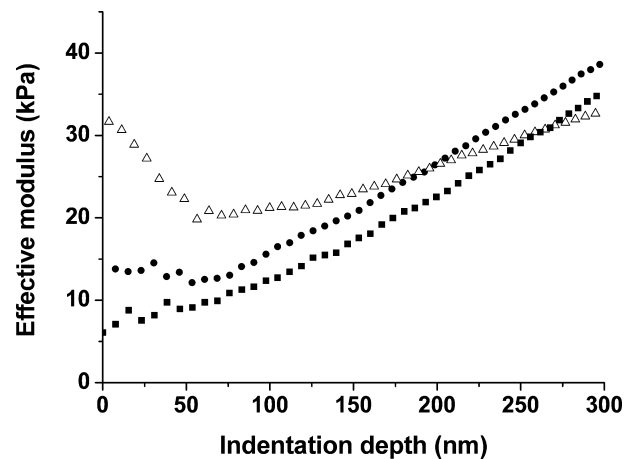
**Fig. 3** Pointwise effective modulus  $E^* = E_Y / (1 - \nu^2)$  of articular cartilage as a function of indentation depth, calculated at each data point of the indentation depth versus indentation load curve with the indentation depths of (a) up to 300 nm and (b) up to 600 nm

#### 2.4 Microscale mechanical response of articular cartilage

AFM indentation tests were performed on the cartilage sample with  $Z$  limits of 2.5 V and 20 V at 1 Hz and 9.3 Hz loading frequencies. The microscale  $E_Y$  was also calculated for each indentation curve using the same method explained above over the indentation depths up to  $D = 300$  nm ( $Z$  limit, 2.5 V) and  $D = 600$  nm ( $Z$  limit, 20 V) at 1 Hz and 9.3 Hz loading frequencies.

#### 2.5 Macroscale unconfined compression experiment (macroscale $E_Y$ of agarose gel)

The custom-designed testing apparatus consisted of a voice-coil force actuator (model LA17-28-000A; BEI



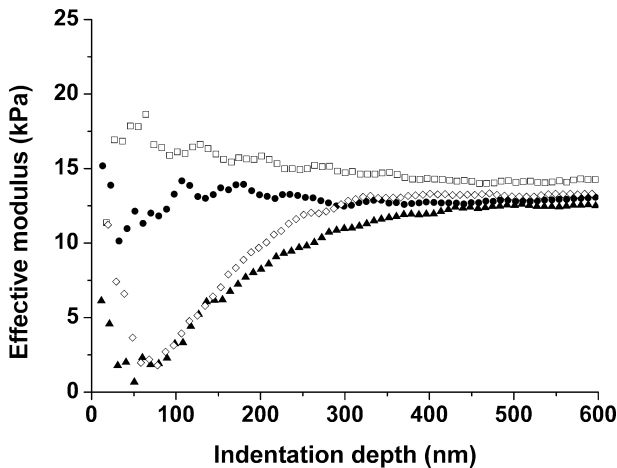
**Fig. 4** Initial behaviour of the pointwise effective modulus  $E^*$  categorized by three types of response (depth-dependent initial increase, decrease, and initially almost depth-independent constant response) from AFM indentation measurements on articular cartilage with an indentation depth of up to 300 nm at 1 Hz loading frequency

Kimco Magnetics Division, USA; 71 N peak force), connected in series with a linear variable-differential transformer for displacement measurements (model PR812-200, Schaeviz Sensors, USA;  $\pm 5$  mm), a loading platen consisting of glass 1 mm thick, the tissue sample, and a stainless steel specimen chamber mounted on a load cell (model 8523, Burster, USA;  $\pm 200$  N). The force actuator, connected to a power supply (model PST-040-13-DP, Copley Controls Corp., USA; +40 V d.c. at 13 A continuous) and controller box (model TA115, Trust Automation INC., USA; 150 W continuous, 325 W peak) was controlled via a force feedback loop using a desktop computer with a data input and output board (model PCI-MIO-16XE-10, National Instruments, USA) running the LabView software package (version 6.1, National Instruments, USA).

2 per cent and 3 per cent agarose gels (diameter 8 mm;  $h = 1.4$  mm) were mounted on a PBS-filled testing chamber, and the specimen was allowed to equilibrate for 4.4 h under a tare load of 0.2 N (equivalent to 4.0 kPa). The reductions in thickness resulting from tare load application were 47.9 per cent for 2 per cent agarose gel and 21.8 per cent for 3 per cent agarose gel. The macroscale  $E_Y$  values of 2 per cent and 3 per cent agarose gels were determined from the applied tare load divided by the reduction in thickness.

#### 2.6 Statistical analyses

One-way analysis of variance (ANOVA) was performed to investigate statistical differences between



**Fig. 5** Pointwise effective modulus  $E^*$  of 2 per cent agarose gel reaching an equilibrium value after the depth-dependent and/or almost depth-independent initial behaviours (indentation depth, 600 nm; loading frequency, 1 Hz)

the microscale  $E_Y$  values of 2 per cent and 3 per cent agarose gels (SAS Institute Inc., USA). Similarly, two-way ANOVA with repeated measures was used to investigate the effects of indentation depths (300 nm and 600 nm) and loading frequencies (1 Hz and 9.3 Hz) on the microscale  $E_Y$  of articular cartilage; post-hoc testing of the means was performed with Bonferroni adjustment [31, 32]. In all cases,  $\alpha$  was set at 0.05 and the significance was set at  $p < 0.05$ .

### 3 RESULTS

The microscale Young's moduli  $E_Y$  of 2 per cent and 3 per cent agarose gels up to 600 nm indentation depth at 1 Hz loading frequency were  $9.3 \pm 2.3$  kPa ( $n = 100$ ) and  $17.5 \pm 3.0$  kPa ( $n = 100$ ) respectively, and similar to their macroscale  $E_Y$  values (2 per cent agarose gel, 8.3 kPa; 3 per cent agarose gel, 18.3 kPa). 3 per cent agarose gel was much stiffer than 2 per cent agarose gel based on the statistical differences in the microscale  $E_Y$  values ( $p < 0.001$ ). It was found that the microscale  $E_Y$  values of articular cartilage calculated from AFM indentation tests under the same loading conditions were  $30.9 \pm 14.3$  kPa ( $n = 100$ ).

The pointwise elastic modulus  $E^*$  of agarose gel reached equilibrium values (Fig. 5), while the pointwise  $E^*$  of articular cartilage showed a non-linear increase with an increase in the indentation depth (Fig. 3) after three typical types of the depth-dependent and/or depth-independent initial behaviours (depth-dependent initial increase and decrease, and

initially almost depth-independent constant response) (Fig. 4).

A two-way ANOVA for the factors of indentation loading frequency and indentation depth shows that the microscale  $E_Y$  of articular cartilage increases significantly with an increase in the applied indentation depth at both 1 Hz and 9.3 Hz loading frequencies ( $p < 0.001$ ) (Fig. 3); the indentation depth-dependent  $E_Y$  increased from  $16.4 \pm 6.5$  kPa to  $30.9 \pm 13.5$  kPa at 1 Hz loading frequency and from  $14.9 \pm 6.2$  kPa to  $32.6 \pm 10.3$  kPa at 9.3 Hz loading frequency ( $n = 12$ ) when the indentation depth increased from 300 nm to 600 nm. However, the effect of loading frequency on the microscale  $E_Y$  of articular cartilage was not significant; the microscale  $E_Y$  values at 1 Hz and 9.3 Hz loading frequencies exhibited no statistical differences ( $p = 1.0$ ) (Fig. 3).

### 4 DISCUSSION

The main objective of the present study was to evaluate a more accurate microscale Young's modulus  $E_Y$  of articular cartilage. Experimentally, this was achieved by AFM indentation tests through a non-Hertzian approach [25] with a relatively large spherical atomic force microscope tip. The result that the microscale  $E_Y$  values of 2 per cent and 3 per cent agarose gels (about 9.3 kPa and about 17.5 kPa respectively) are similar to the macroscale  $E_Y$  values of 2 per cent and 3 per cent agarose gels (about 8.3 kPa and about 18.3 kPa respectively) supports accurate measurements of the microscale  $E_Y$  values. The microscale  $E_Y$  of articular cartilage evaluated from this AFM technique was approximately 30.9 kPa. This value may seem to be relatively small when compared with the macroscale  $E_Y$  of bovine cartilage. However, when the depth-dependent inhomogeneous behaviour of articular cartilage is considered, the microscale  $E_Y$  is in good agreement with the macroscale  $E_Y$  of articular cartilage. On a macroscale,  $E_Y$  has been reported to be about 490 kPa when bovine cartilage was compressed by a deformation of about 200  $\mu\text{m}$  from approximately 1.83 mm thickness [33]. This depth-dependent  $E_Y$  has further decreased to about 100 kPa when investigated within 5 per cent of the full-thickness depth from the articular surface under an average tissue compressive strain of 10 per cent by optical measurements methods and digital image analysis [34, 35]. Accounting for the magnitude of the 600 nm indentation depth of this study, it seems reasonable to conclude that AFM measurements of  $E_Y$  at the ultrathin surface layer of articular cartilage are

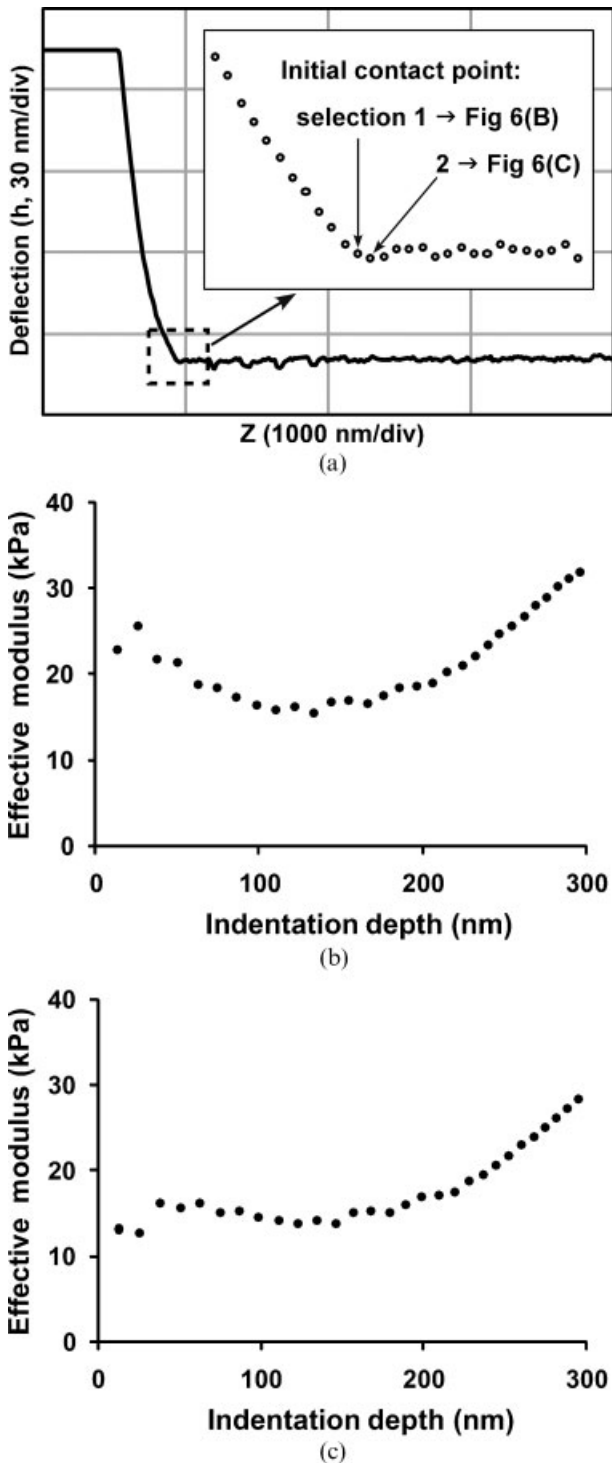
consistent with these previous findings. However, this conclusion is based on comparisons between the microscale  $E_Y$  of the current study obtained from unfrozen samples and the macroscale  $E_Y$  of the literature calculated from frozen samples. Although the previous study has shown that freezing of articular cartilage for 24 h has no significant effect on microscale surface roughness and superficial structure, it will be important to measure directly the effect of the freezing period of articular cartilage on the microscale  $E_Y$  as well as its relationships with the surface roughness and superficial structure of articular cartilage.

From the theoretical analysis of articular cartilage based on the biphasic theory [36], the characteristic time constant  $\tau = a^2/H_A k$  on the macroscale which explains the time-dependent decrease in interstitial fluid load support of articular cartilage [37–39] yields 2051 s using the representative material properties of immature bovine cartilage from a previous study by two of the present authors [40], where the radius of the contact area is  $a = 4$  mm, the aggregate tensile modulus of the solid matrix is  $H_A = 13$  MPa, and the hydraulic permeability is  $k = 0.6 \times 10^{-15} \text{ m}^4/\text{N s}$ . On a microscale, however, because of the very small size of the atomic force microscope indenter tip,  $a = 2.5 \mu\text{m}$ , the time constant is equal to 0.8 ms. Consequently, interstitial fluid pressurization will subside very rapidly in AFM indentation measurements with applied loading frequencies of 1 Hz and 9.3 Hz, and the microscale  $E_Y$  of articular cartilage of this study corresponds to the intrinsic (fluid-independent) property of cartilage solid phase independently of the effect of its fluid phase.

This study was also aimed at characterizing the microscale mechanical response of articular cartilage by applying microscale strains ranged within the regions of lamina splendens (the ultrathin layer of the articular surface within 5–10  $\mu\text{m}$ ) of articular cartilage. On a macroscale, a previous study by two of the present authors and a co-worker [33] has reported that fluid-dependent viscoelasticity and non-linearity of articular cartilage play an important role in providing cartilage with the functional properties that allow it to sustain the severe loading environment in joints. However, in this study, calculation of the pointwise  $E^*$  at each data point of the AFM indentation depth–force curve was performed under the assumption that the microscale behaviour of articular cartilage would be elastic, and the result that the microscale  $E_Y$  values at 1 Hz and 9.3 Hz loading frequencies were not significantly different did not contradict this elastic assumption

of articular cartilage for a microscale deformation of less than 600 nm.

Another important finding of this study was that statistically significant differences between the microscale  $E_Y$  values of articular cartilage calculated by averaging its pointwise  $E^*$  over the indentation depths of either 300 nm or 600 nm were observed between these two deformation levels (300 nm and 600 nm). This observation of the indentation depth-dependent cartilage microscale  $E_Y$  is consistent with the macroscale inhomogeneous behaviour of articular cartilage [33, 41]. According to the study by Krishnan *et al.* [41], the assumption of an inhomogeneous cartilage layer to loading shows more increase in the interstitial fluid load support than the homogeneous assumption and results in the enhancement of the friction and wear properties of articular cartilage from finite element method on a macroscale. While new information on the microscale mechanical properties of articular cartilage has been provided from this study, it is important to outline the limitations of this study. Although 100 AFM indentation measurements of the microscale  $E_Y$  values for 2 per cent and 3 per cent agarose gels were performed, no statistical analysis between the microscale and macroscale  $E_Y$  values was conducted because only one measurement of the macroscale  $E_Y$  values for 2 per cent and 3 per cent agarose gels was performed with the assumption of consistent macroscale behaviour for agarose gel based on its homogeneous structure, which is a limitation of this study. Another limitation of this study is that different selections of the initial contact points between the atomic force microscope tip and sample surface from even the same approaching signal of AFM indentation loading affect the initial behaviour of the pointwise  $E^*$  of articular cartilage (Fig. 6). Although the ideal contact points between the atomic force microscope tip and cartilage surface were determined by employing a two-part polynomial model-fitting algorithm of the literature in order to minimize the examiner's subjective judgements [25], the initial responses of the pointwise  $E^*$  values were not consistently the same, showing three types of behaviour (depth-dependent initial increase and decrease, and initially an almost depth-independent constant response) (Fig. 4). Because the initial depth-dependent decrease in the pointwise  $E^*$  of articular cartilage is clearly different from its overall depth-dependent increase (i.e. statistically significant differences between the average values of the pointwise  $E^*$  over 300 nm and 600 nm indentation depths), it is a limitation of this study caused by the



**Fig. 6** (a) Different selections (selections 1 and 2) of the initial contact points between the atomic force microscope tip and sample surface from the same approaching signal of AFM indentation loading (indentation depth, 300 nm; loading frequency, 1 Hz) which affect the initial behaviour of the pointwise effective modulus  $E^*$  of articular cartilage. (b) Depth-dependent initial decrease and then increase for selection 1 of the contact point. (c) Almost depth-independent constant initial response for selection 2 of the contact point

dependence on the selections of the initial contact points between the atomic force microscope tip and sample surface from AFM indentation data. However, it is believed that this limitation could be overcome to some extent by the averaging method of the pointwise  $E^*$  values over the indentation depth of 300 nm and/or 600 nm to calculate the microscale  $E_Y$ .

In summary, this study reports more accurate measurements of the microscale mechanical response of articular cartilage from AFM indentation which can be adopted for assessing microscale mechanical properties in tissue-engineered cartilage and designing microscale structures of chondrocyte-seeded scaffolds. In future studies, it is planned to use the experimental results of this study to formulate a constitutive relation which accounts for the observed depth-dependent and frequency-independent behaviour on a microscale, and further to extend to the investigation the effect of cytokines (i.e. IL-1 and TNF- $\alpha$ ) on the microscale properties of chondrocytes and collagen fibrils of articular cartilage.

#### ACKNOWLEDGEMENTS

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